# Sulfur Poisoning and Regeneration of Pd Catalyst under Simulated Emission Conditions of Natural Gas Engine

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#### ABSTRACT

Palladium-based catalyst can be employed for natural gas exhaust clean up due to its high activity for light hydrocarbon oxidation. Unfortunately, trace amounts of sulfur in the natural gas feed severely deactivate the catalyst.

In this paper, SO<sub>2</sub> adsorption over a monolithic Pd/Al<sub>2</sub>O<sub>3</sub> oxidation catalyst is monitored in a time-resolved manner in the presence of 100 ppm SO<sub>2</sub> under simulated aging conditions of a natural gas engine, which is correlated with the oxidation activity for CO and hydrocarbons such as CH<sub>4</sub>, C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub>. The SO<sub>2</sub> adsorption is saturated in 0.5 h at 400 °C and 100,000 h<sup>-1</sup>. The molar ratio of adsorbed SO<sub>2</sub> and Pd is about 2/1, indicating SO<sub>2</sub> molecules adsorbed, or transferred to the Al<sub>2</sub>O<sub>3</sub> support. The oxidation activity gets stabilized upon saturation of sulfur adsorption, and the hydrocarbon oxidation activity removed from the stream. The light-off temperatures (T<sub>50</sub>) of hydrocarbons shift 50-100 °C higher after SO<sub>2</sub> poisoning.

When the gas stream was switched to the fuel-rich mode, 15% of the adsorbed  $SO_2$  molecules were released from the poisoned catalyst at 400 °C. No H<sub>2</sub>S was detected in the outlet stream in the reducing atmosphere. Only traces of  $SO_2$  molecules were detected when the regenerating temperature increased to 550 °C. The poisoned Pd catalyst was reactivated to some degree, but suffered from a significant deactivation in 30 min even in the absence of  $SO_2$ , regardless of regenerating temperature. The results revealed the existence of reversible and irreversible sulfur in the reducing atmosphere. A mechanism of sulfur poisoning and regeneration is proposed.

#### INTRODUCTION

Natural gas engines are in high demand and are used in many applications such as power generation, gas compression, and cogeneration. The driving forces include economical, political, and environmental factors. Natural gas used to be a relatively cheap primary energy source, always at a discount to crude oil (on a

comparative British thermal unit basis). It gradually evolved into a major resource during the 20th century reaching a 24 per cent share of global primary energy in 1999. In the year 2000, natural gas prices in the USA rose to unheard-of highs of \$10/million Btu, ushering in a new era, with natural gas at a 120 percent premium to crude oil [1]. Due to the political instability in middle east and other oil-producing areas, the diversification of energy sources is encouraged by government. Furthermore, spark-ignited lean burn natural gas engines have significant environmental advantages over rivals of gasoline and diesel fuel, such as lower  $NO_x$  and  $SO_x$ emissions, fewer particulate matters. CO<sub>2</sub> emissions are also reduced because H/C ratio of natural gas is about double that of gasoline and diesel fuel [2].

The drawback of natural gas engines is the emissions of non-combusted methane and non-methane hydrocarbons (NMHCs). Methane is known to be a powerful greenhouse gas with about 20 times the greenhouse potential of carbon dioxide. The environmental impact of methane and NMHCs is being reflected in present and future regulations. At least 60% methane conversion is required to meet the most stringent current European regulations for THC limit values (Tier Euro IV, effective from October 2005) [2].

Palladium-based catalysts are discovered to be the most active for methane and NMHCs abatement [2]. The ease of oxidation of alkane hydrocarbons is related to carbon numbers, e.g. larger molecules are more vulnerable to attack by oxygen. Thus, methane is the toughest hydrocarbon molecule to activate. The additional factors of the presence of large amounts of water (5%-10%), low temperatures (400-450 °C), and traces of sulfur dioxide (1ppm) in the engine exhaust create the greatest challenge to the Pd based catalysts [3]. Hydrothermal aging and phosphorous poisoning are contributors to catalyst deactivation. However, this paper focuses on sulfur poisoning. Phosphorous compounds are typically strong poisons and may be introduced from additives of lubricating oils used in pumps, blowers, fans and other machineries. Work by McCormick et al shows that Pd/Al<sub>2</sub>O<sub>3</sub> catalyst deactivated in less than 50 hours in lean burn gas engine exhaust [4]. It is well known that the active site of hydrocarbon oxidation is PdO particles

[5]. SO<sub>2</sub> converts to SO<sub>3</sub> by PdO with excess oxygen in the gas stream, and PdO reacts with SO<sub>3</sub> to form less active PdO-SO<sub>3</sub>. Complete poisoning of the PdO is retarded with the use of a sulphating support, such as Al<sub>2</sub>O<sub>3</sub>. The support is capable of adsorbing sulphur and buffering the poisoning onto the PdO particle. On the contrary, a non-sulphating support such as SiO<sub>2</sub> cannot act as a SO<sub>3</sub> reservoir, and PdO is poisoned rapidly and directly by SO<sub>3</sub>. Sulphur-aged Pd catalysts can be partly regenerated under reducing atmosphere such as H<sub>2</sub> [5-8].

Few works have been published regarding the sulfur adsorption and desorption on Pd-based catalysts under lean burn natural gas engine conditions. Recently temperature programmed reduction (TPR) tests of SO<sub>2</sub>-aged Pd/Al<sub>2</sub>O<sub>3</sub> powder catalyst were conducted in flowing CH<sub>4</sub>, 2% H<sub>2</sub>O and He [7]. SO<sub>2</sub> release was observed between 400-700 °C by mass spectrometer.

The objective of this work is to investigate the  $SO_2$  adsorption and desorption under exhaust conditions of natural gas engines. This knowledge would help to better understand the mechanism of sulphur poisoning and regenerating of Pd catalysts. The sulphur adsorption over a monolithic Pd-based oxidation catalyst is monitored in a time-resolved manner in the presence of  $SO_2$  under simulated emission conditions of natural gas engine, which is correlated with the oxidation activity for CO and hydrocarbons such as  $CH_4$ ,  $C_2H_6$  and  $C_3H_8$ . In order to regenerate the catalyst, the gas stream was changed to reducing atmosphere. The sulphur release was examined at different temperatures and correlated with effectiveness of the catalyst regeneration.

# EXPERIMENTAL

The Pd-based catalyst is supported on 400cpsi cordierite substrate with an  $Al_2O_3$  washcoat. The Pd loading is 5 g per litre substrate (142 g/ft<sup>3</sup>). Catalyst cores with a diameter of 1.0 cm and volume of 3.5 cm<sup>3</sup> were used to fit the stainless steel reactor.

Catalytic performance was tested in a conventional stainless-steel tubular reactor that is described in a previous paper [9]. Gas compositions used are listed in Table 1 and the gas mixture was fed to the reactor with a space velocity of 100,000 h<sup>-1</sup> @STP based on substrate volume unless otherwise specified. The catalyst is located in the isothermal zone of the reactor. The gas temperature at the inlet was recorded as the reaction temperature. Light off curves were collected by increasing the reaction temperature from 100 to 500 °C. Gas composition was monitored in a time-resolved manner using a Fourier Transform Infra Red spectrometer (FTIR) manufactured by MKS Instruments.

 $SO_2$  poisoning is performed by exposing the catalyst to 100 ppm  $SO_2$ . High concentrations of  $SO_2$  are used to rapidly age the catalyst and simulate sulphur exposure of the catalyst to 1 ppm S for 100 hours. The fresh catalysts were poisoned at 400 °C by introducing 100 ppm  $SO_2$  to

the lean gas composition reactant stream. The  $SO_2$  poisoning generally takes less than 1 h for the oxidation activity to reach a steady state.

After  $SO_2$  poisoning and light-off curve collection, the catalyst was regenerated in a reducing atmosphere. The gas composition of regeneration is listed in Table 1. During the regeneration, oxygen was switched to N<sub>2</sub> with the same flow rate. The regeneration continued until no sulphur dioxide was released from the catalyst, which generally takes half an hour.

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Component	Lean	Regeneration
CH <sub>4</sub>	1000 ppm	1000 ppm
C <sub>2</sub> H <sub>6</sub>	150 ppm	150 ppm
C <sub>3</sub> H <sub>8</sub>	50 ppm	50 ppm
CO	1000 ppm	1000 ppm
NO	100 ppm	100 ppm
O <sub>2</sub>	10%	0
H <sub>2</sub> O	5%	5%
CO2	5%	5%
SO <sub>2</sub>	0*	0
N <sub>2</sub>	Balance	Balance

Table 1. Model gas composition (SV =  $100,000 \text{ h}^{-1}$ ).

Note: \*SO<sub>2</sub> is around 100 ppm during poisoning. The regeneration was only performed in reducing atmosphere.

The fresh and regenerated catalyst samples were characterized with Transmission Electron Microscopy and Energy Dispersive X-Ray Spectrometry (TEM/EDS) in order to obtain Pd particle size information and sulfur content.

#### **RESULTS AND DISCUSSION**

Four catalyst cores (samples) were cut from the same piece of catalyst monolith and used in this work in order to characterize the samples with different conditions. The reaction conditions over various samples are listed in Table 2. The term 'light-off curve' in Table 2 means that a light-off curve was collected from 100 to  $500^{\circ}$ C.

Table 2. Reaction conditions	over various samples.
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Steps	Sample 1	Sample 2	Sample 3
1	Fresh	Fresh	Fresh
2	Light-off curve	Light-off curve	1h SO <sub>2</sub>
3	1h SO <sub>2</sub>	1h SO <sub>2</sub>	1h/400℃ regeneration
4	Light-off curve	Light-off curve	1h/400℃ regeneration
5	39 h SO <sub>2</sub>	1h/400℃ regeneration	400-550 ℃ regeneration
6	Light-off curve	TEM/EDS	Light-off curve
7			TEM/EDS

The oxidation activity of Palladium catalyst was evaluated when fresh and after  $SO_2$  poisoning. Figure 1

displays the light-off curves of methane, ethane and propane over the fresh and poisoned catalyst. The lightoff curves were collected when the catalyst was fresh, after poisoning for 1 h at 400 °C by 100 ppm SO<sub>2</sub>, and after 40 h aging by SO<sub>2</sub> under the same conditions. During reaction conditions, the fresh catalyst sample is found to be deactivating slowly even in the absence sulfur dioxide, likely due to the presence of water in the stream [10]. The deactivation of the catalyst is greater after SO<sub>2</sub> poisoning. The catalyst was seriously poisoned by SO<sub>2</sub> during the first hour in the stream. The light-off temperatures of methane, (T<sub>50</sub>) over aged catalyst are 100°C higher than fresh. Catalytic activity has reached steady state during the first hour, because no further deactivation is observed with longer exposure times (up to 40 hours) to high SO<sub>2</sub> concentrations.

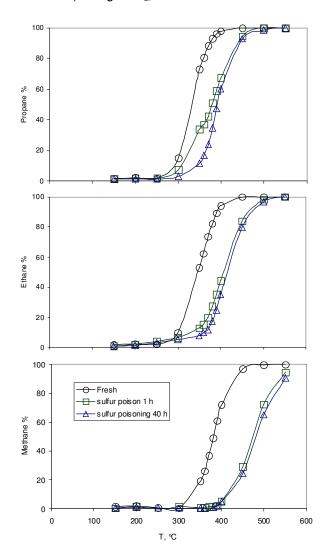


Figure 1. Light-off curves of methane, ethane and propane over Pd-based monolithic catalyst before and after aging.  $SV=100,000 h^{-1}$ .  $SO_2$  aging conditions: 100 ppm  $SO_2$ , 400 °C, the other components see Table 1.

The extent of light-off shift after  $SO_2$  exposure depends on the type of hydrocarbon component. While  $T_{50}$  of methane after  $SO_2$  aging moves 100 °C higher relative to the fresh, light-off temperatures of ethane and propane shift 65 °C and 50 °C, respectively. This is consistent with Pd catalyst aging test results on a lean burn natural gas engine [4]. These authors report the deactivation of PdO by sulfur oxides is due to both a decrease in the chemisorption of hydrocarbons on PdO-SO<sub>x</sub> and a decrease in the availability of oxygen from PdO-SO<sub>x</sub> [5]. The PdO-SO<sub>x</sub> sites are still active in propane oxidation, but not sufficient to activate methane molecules. Therefore, the light-off shift of propane is not so far as methane after SO<sub>2</sub> poisoning.

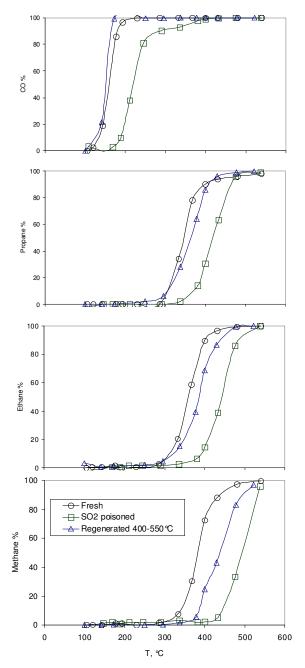


Figure 2. Light-off curves of CO, methane, ethane and propane over Pd-based catalyst when fresh,  $SO_2$  aged or regenerated. SV=100,000 h<sup>-1</sup>.

Figure 2 shows the catalytic performance of the catalyst sample that has been regenerated under reducing atmosphere for 3 h between 400-550 °C. During

regeneration, the oxygen flow is replaced by nitrogen to maintain a constant flow rate and space velocity through the catalyst. The catalyst was regenerated first at 400 °C for 2 h, and then the temperature is ramped at 10 °C/min to 550 °C for 1 h. The activity is recovered completely for CO oxidation, mostly for propane and ethane, but only half for methane oxidation. The recovery dependence on compounds indicates that some sulfur residue may exist in the catalyst and interact with Pd particles.

As shown in Table 2, a series of treatments have been undertaken to investigate the catalytic performance of various catalyst conditions. The catalyst samples were treated under various conditions step by step, followed by activity measurements at 400 °C after each step: (a) Fresh catalyst; (b) During SO<sub>2</sub> poisoning at 400 °C; (c) After 1h SO<sub>2</sub> poisoning; (d) Regenerating at 400 °C for 1 h; (e) Regenerating at 400 °C for another 1 h; (f) Regenerating at 550 °C for 1 h. In order to check the reproducibility, the catalyst sample was replaced by a new one of the same batch after step (e), and the steps (a)~(e) were repeated. It was observed that the results of activity and SO<sub>2</sub> adsorption/desorption are reproducible. Some samples were characterized using TEM/EDS.

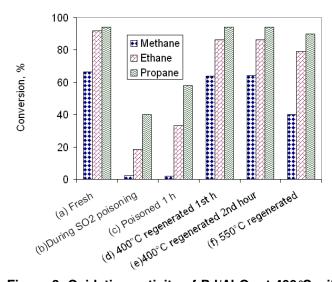


Figure 3. Oxidation activity of  $Pd/Al_2O_3$  at 400 °C with different catalyst conditions. The presented conversions after regeneration are collected immediately after regenerating.

Figure 3 shows the hydrocarbon conversions at 400 °C for an overall comparison. It is noted that activity was recorded in the presence of 100 ppm SO<sub>2</sub> at steady state after 50 min poisoning for step (b). After regeneration at 400 °C, the oxidation activity of the catalyst is almost fully recovered. However, the increase in regeneration temperature to 550 °C does not help. No remarkable activity recovery is observed after removing the 100 ppm SO<sub>2</sub> from the gas steam, indicating an irreversible deactivation by SO<sub>2</sub> at 400 °C under oxidizing atmosphere. It appears that the activity keeps constant at 400 °C for at least 40 h after SO<sub>2</sub> poisoned even without sulphur in the stream.

After regeneration at 400 °C or 550 °C, some of the oxidation activity is recovered for a very short time. The activity decreases rapidly even in the absence of SO<sub>2</sub> in the stream, and is particularly pronounced for methane oxidation (Figure 4). The methane conversion decreases from 60% to 30% in less than one hour. For the same duration, the ethane conversion decreases from 88% to 72%, and only a negligible activity loss is observed for propane oxidation, from 93% to 87% in conversion. This activity loss is a typical symptom of SO<sub>2</sub> deactivation as discussed above and is indicating that sulfur transfers from the support to the Pd particles.

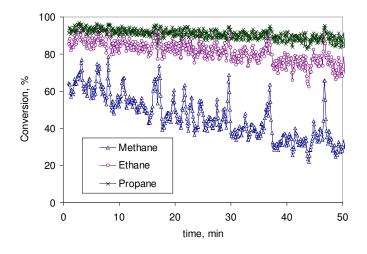


Figure 4. The hydrocarbon conversions decreased rapidly after regenerating at 400  $^{\circ}$ C even though the gas stream contained no SO<sub>2</sub>.

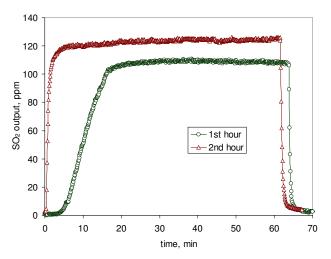


Figure 5. SO<sub>2</sub> adsorption during the first and second hour of poisoning. The catalyst was purged 30 min after the first hour of SO<sub>2</sub> poisoning. SV=100,000 h<sup>-1</sup>. SO<sub>2</sub> aging conditions: 1<sup>st</sup> hour 105 ppm SO<sub>2</sub>, 2<sup>nd</sup> hour 120 ppm; 400 °C.

The SO<sub>2</sub> adsorption on the Pd catalyst is saturated within 10-30 min, as revealed in Figure 5. From Figure 1, the catalyst deactivation derived from 100 ppm SO<sub>2</sub> poisoning peaks in the first hour. One separate test was conducted to study the SO<sub>2</sub> adsorption during first and

second hour of SO<sub>2</sub> poisoning. The inlet SO<sub>2</sub> concentration during the first hour (105 ppm) is slightly different from the second hour (120 ppm). The catalyst was purged 30 min in the gas stream without SO<sub>2</sub> after the first hour of poisoning until the outlet SO<sub>2</sub> concentration reached zero. The Pd-based catalyst does not catalyze SO<sub>2</sub> oxidation to SO<sub>3</sub>, at least after the catalyst is poisoned by SO<sub>2</sub>. In the first hour of poisoning, the SO<sub>2</sub> concentration at exit increased from 0 to 105 ppm while the input SO<sub>2</sub> concentration remained constant at 105 ppm or so. It indicates that SO<sub>2</sub> adsorption was saturated during the first hour under the specified conditions. The SO<sub>2</sub> concentration at exit was determined during the second hour of poisoning. The SO<sub>2</sub> output reached 120 ppm in 5 min. The SO<sub>2</sub> accumulation is around zero during the second hour of poisoning. It is demonstrated that the SO<sub>2</sub> adsorption is saturated during the first hour of poisoning at 400 °C.

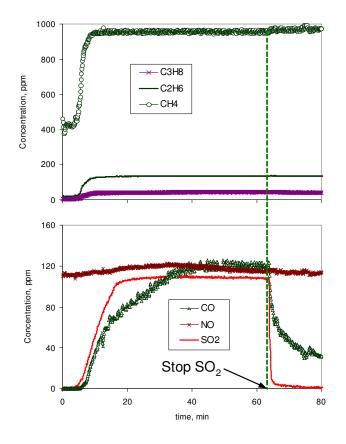


Figure 6. SO<sub>2</sub> adsorption and activity change (outlet concentration) during the first hour of poisoning. SO<sub>2</sub> aging conditions: 110 ppm SO<sub>2</sub>, 400 °C.

The SO<sub>2</sub> accumulation in the catalyst is calculated based on the difference of input and output SO<sub>2</sub> concentrations in the gas stream. The molar ratio of accumulated SO<sub>2</sub> and palladium is about 2/1. It should be noted that the SO<sub>2</sub> exposure in this paper was conducted under engine emission conditions in the presence of H<sub>2</sub>O, NO<sub>x</sub> and 100 ppm SO<sub>2</sub>. 100 ppm SO<sub>2</sub> was used in this work to accelerate the poisoning. The SO<sub>2</sub> concentration is not engine emission conditions, but it is a good simulation of long-term exposure to 1 ppm sulfur. The activity of poisoned catalyst is generally higher than the field aged catalyst based on our experience, due to other contaminants and factors in the engine emissions [11]. After SO<sub>2</sub> poisoning, sulfate formation occurs only on the external surface of PdO<sub>x</sub> particles, and the PdO<sub>x</sub> particles contains some Pd metal even though the SO<sub>2</sub> exposure takes place in excess oxygen [12]. XPS analysis was conducted on unsupported PdO<sub>x</sub> that had been exposed to SO<sub>2</sub> or SO<sub>3</sub> in air at 400 °C or 520 °C [5,12]. It was found that the maximum S/Pd atom ratio is 0.23 over unsupported PdO<sub>x</sub> which is much smaller than the ratio of 2 observed here. It suggests that most of the adsorbed sulfur transported from PdO<sub>x</sub> particles to the support.

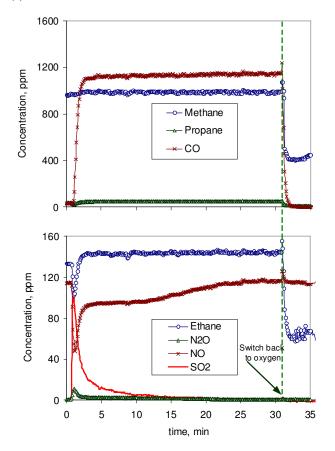


Figure 7. Transient-state study (outlet concentration) during the regeneration of sulphur-aged  $Pd/Al_2O_3$  catalyst. Oxygen was replaced by N<sub>2</sub> with the same flow rate during the regeneration at 400 °C. The gas was switched back to oxidizing atmosphere at 30.5 min as shown in the figure.

The concentrations of the other gas components were monitored during the  $SO_2$  exposure using the gas analyzer, as shown in Figure 6. The concentrations of methane, ethane and propane increased dramatically during the initial 10 minutes of  $SO_2$  exposure, and stabilized quickly in 10 minutes. After stopping  $SO_2$ introduction, hydrocarbon concentrations were little changed. The results show that the hydrocarbon oxidation activity remains constant once sulfur adsorption is saturated, regardless of the  $SO_2$ concentrations afterwards in the gas stream. However, the CO concentration increased from 0 to 120 ppm during the initial 40 min, and decreased to 35 ppm in 20 min after stopping SO<sub>2</sub> introduction. The SO<sub>2</sub> molecules may compete for PdO<sub>x</sub> or PdSO<sub>4</sub> sites. It is worthy to compare the SO<sub>2</sub> adsorption and activity of hydrocarbon oxidation. The outlet reactor concentrations of all the three hydrocarbons reached their maximum points during the first 10 min, while SO<sub>2</sub> concentration was only 50 ppm at the same time. It took an extra 10 min for the SO<sub>2</sub> to reach its maximum concentration, 110 ppm. The difference implies that SO<sub>2</sub> molecules adsorb and convert selectively on the PdO<sub>x</sub> particles, and spillover to the surrounding Al<sub>2</sub>O<sub>3</sub> surface.

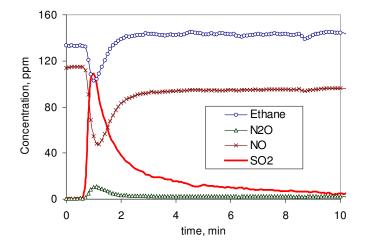


Figure 8. Transient-state study (outlet concentration) during the regeneration of sulphur-aged  $Pd/Al_2O_3$  catalyst. Oxygen was replaced by  $N_2$  with the same flow rate during the regeneration at 400 °C.

The SO<sub>2</sub> release from the catalyst was observed while the gas stream was switched to reducing atmosphere, presented by Figure 7. The transient SO<sub>2</sub> release occurs in the first few minutes of oxygen removal, a zoomed in view of this region is shown in Figure 8. It should be noted that no H<sub>2</sub>S release was detected during the regeneration. The SO<sub>2</sub> release during reducing atmosphere is further evidence that the sulfur exists in the form of sulfates on the surface of the catalyst. The release is 15% of the accumulated SO<sub>2</sub> during poisoning. As mentioned above, the maximum S/Pd ratio in PdOx particles is 0.23. The SO<sub>2</sub> release is equivalent with the S/Pd ratio of 0.3, indicating that only the sulfates on the PdO<sub>x</sub> particles and vicinity were reduced at 400 °C in the reducing atmosphere. It is also interesting to notice the changes of other components during the transient state. All of the hydrocarbons and NO exhibit inverse peaks, probably due to the reactions between them. During the transition from oxidizing to reducing atmosphere, there was a stoichiometric point at which NO may react with hydrocarbons. Another evidence for the NO reduction is the release of N<sub>2</sub>O during the transition. N<sub>2</sub>O is generally recognized as a product of NO reduction.

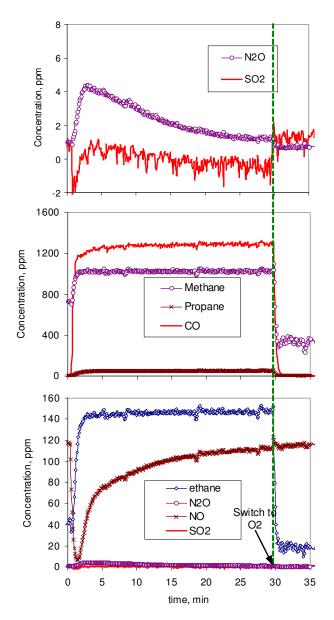


Figure 9. Transient-state study (outlet concentration) during the  $2^{nd}$  time regeneration of sulphur-aged Pd/Al<sub>2</sub>O<sub>3</sub> catalyst. Oxygen was replaced by N<sub>2</sub> with the same flow rate during the regeneration at 400 °C.

Figure 9 presents the concentration changes during the second regeneration at 400 °C in the reducing atmosphere. As shown in Figure 4, the catalytic activity deteriorates quickly after regeneration. It is suspected that  $SO_4^2$  species transfer from the support to  $PdO_x$ particles and lead to a fast deactivation. After one hour of purging in the oxidizing atmosphere, oxygen was replaced again by nitrogen. The concentrations of hydrocarbons, CO and NO<sub>x</sub> went through the similar changes to the first regeneration at 400 ℃. From the top part of the Figure 9, only a trace of SO<sub>2</sub> was detected at the outlet. It reveals that a small amount of sulfur migrates from the support Al<sub>2</sub>O<sub>3</sub> to the sulfur-free PdOx particles. It is consistent with the previous studies [13]. TPD and activity studies by Gelin et al suggest that, while not being completely removed from the catalyst, sulfate species can migrate back and forth between PdO and

alumina sites, depending on the temperature, therefore preventing the complete regeneration of the catalyst. The activity was almost fully recovered at the beginning, indicating the remarkable impact of traces of sulfates at the surface of the  $PdO_x$  particles. However, the regenerated catalyst suffered from a quick deactivation with respect to methane activation, as shown in Figure 4.

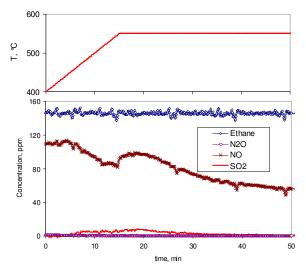


Figure 10. Transient-state study (outlet concentration) during the temperature-programmed regeneration of sulphur-aged Pd/Al<sub>2</sub>O<sub>3</sub> catalyst. The catalyst had been regenerated at 400 °C for 2 hours prior to temperature increasing. The temperature increased from 400 °C to 550 °C at ramping rate of 10 °C/min.

The regenerating temperature was ramped to 550 ℃ to check if more SO<sub>2</sub> would be released from the catalyst sample (Figure 10). As mentioned above, the SO<sub>2</sub> aged sample had been regenerated 2 h at 400 ℃. Prior to ramping the temperature, the gas stream was changed to reducing atmosphere and the catalyst purged for 30 min. The temperature increased from 400 °C to 550 °C at a rate of 10℃/min. The temperature is limited at 550℃ because Pd may sinter at higher temperatures and in the reducing atmosphere [14,15]. SO<sub>2</sub> molecules were detected at the outlet with a very broad peak. As mentioned above, sulfates on the PdOx particles had been reduced at 400℃, or before the temperature increase from 400 °C to 550 °C. This part of released SO<sub>2</sub> was likely originated from the alumina rather than PdO<sub>x</sub> sites. The slow SO2 release indicated that sulfate species at the alumina sites needed to migrate to PdO<sub>x</sub> sites in order to be reduced. The reducing rate is likely limited by the strong resistance of mass transfer from the  $Al_2O_3$  surface to  $PdO_x$  particles. The amount of  $SO_2$ release here is about 10% of the total adsorption during SO<sub>2</sub> poisoning. In addition to the SO<sub>2</sub> release of the previous regenerations at 400 °C, the total SO<sub>2</sub> release is around 25% of the accumulated sulfur in the catalyst.

Energy Dispersive X-Ray Spectrometry (EDS) reveals the existence of the sulfur after the regenerations in Figure 11. A strong sulfur peak can be observed after regenerations at 400  $^{\circ}$ C, and the sulfur peak is still

present even after regeneration at 550 °C. There is no sulfur peak in the EDS spectra of the fresh sample. TPR results showed that regeneration of SO<sub>2</sub> aged Pd/Al<sub>2</sub>O<sub>3</sub> started at 350 °C and completed at 800 °C [7]. The regeneration temperature may not be high enough in our research to remove all the sulfur in the catalyst. The TEM images are shown in the Figure 12. The palladium particles are around 10 nm for fresh and regenerated catalysts. Therefore, PdOx species did not sinter significantly with the treatments in this work.

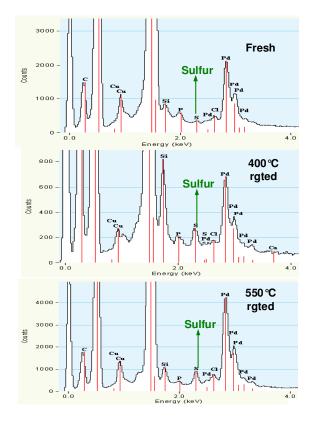


Figure 11. Energy Dispersive X-Ray Spectrometry (EDS) spectra reveals the existence of sulfur even after regeneration.

The mechanisms of poisoning, regeneration and deactivation are illustrated in Figure 13 based on the experimental results. SO<sub>2</sub> oxidation is catalyzed by PdO<sub>x</sub>, forming sulfate species selectively on the surface of PdO<sub>x</sub> particles. The sulfates are believed to transport to alumina sites. Once the neighboring alumina sites are occupied, the adsorption and conversion of SO<sub>2</sub> is very slow or even stopped. Under simulated engine emission conditions, 400 °C and 100,000 h<sup>-1</sup>, it takes about 20 min to reach saturation in the presence of 100 ppm SO<sub>2</sub>. Even removing SO<sub>2</sub> in the stream, the sulfates would not decompose at 400 °C. Sulfates may move and redistribute around the catalyst surface, but the rate depends on temperature and it is likely very slow at 400 °C. When the gas stream changes to rich-burn conditions, the sulfates on PdO<sub>x</sub> particles (PdSO<sub>4</sub>) are immediately reduced to SO<sub>2</sub> that will be released from the catalyst. The sulfate reduction likely happens only on PdO<sub>x</sub> sites at reaction temperatures below 550 °C [16]. The sulfates at the vicinity migrate onto PdO<sub>x</sub> particles and get reduced, but the migration is probably very slow and depends on the temperature. The  $PdO_x$  particles are reduced to Pd metal at 400 °C by CO or hydrocarbons. When the gas stream becomes lean, Pd is oxidized to PdO<sub>x</sub>, and traces of sulfates move onto clean PdO<sub>x</sub> particles. Hydrocarbon oxidation is very sensitive to sulfates, particularly for methane, probably due to the modification of electronic properties by sulfate groups. Even after reduction at 550 °C, significant amount of sulfates still exist in the catalyst.

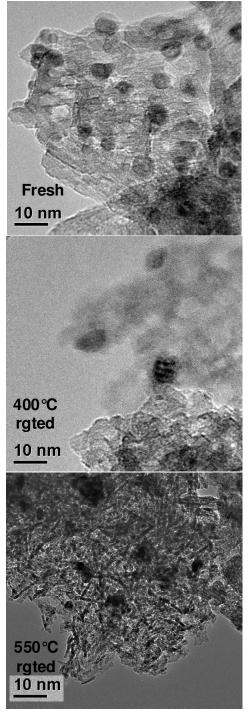
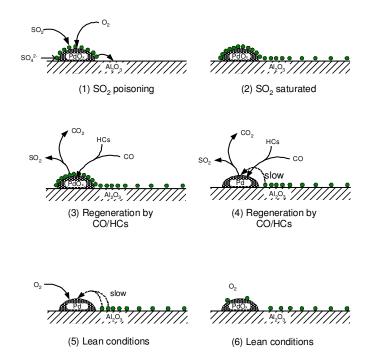


Figure 12. TEM images of catalyst when fresh and regenerated at different temperatures.

The oxidation state of palladium and its effect on oxidation reactions has been extensively studied, and reviewed [17]. It is generally accepted that PdO is the

active site for hydrocarbon oxidation, and metallic Pd is much less active. In oxidizing atmosphere, PdO is stable up to 600-650 °C based on temperature programmed study [18] and thermodynamic calculations [17]. PdO decomposes to less active Pd at temperatures more than 850 °C. After being exposed to high temperatures a re-oxidation takes place when the catalyst is cooled to 650 °C, causing re-dispersion of PdO on alumina as well as the formation of PdO<sub>x</sub>/Pd particles [18]. Temperature programmed oxidation shows that oxidation of Pd<sup>0</sup> (supported on Al<sub>2</sub>O<sub>3</sub>) occurs between 300-450 °C [19]. After rich regeneration, at least a part of Pd<sup>0</sup> converts to PdO at 400-550 °C in the presence of 10% O<sub>2</sub> and NO<sub>2</sub>.

There are some publications on the mechanism for the deactivation of PdO catalysts by sulfur-containing compounds [12]. For the  $SO_2$  poisoning, we agree to the suggestions by Lampert et al and Gelin et al [5, 13].



# Figure 13. Scheme of $SO_2$ poisoning, regeneration, and sulfate re-distribution mechanism for Pd/Al<sub>2</sub>O<sub>3</sub> catalyst.

Regeneration of S-poisoned palladium catalysts with reducing atmosphere was studied in the literature [3,6-8, 15]. Lampert et al proposed an operating strategy of NGV engines based on alternative long periods (14 min) of lean conditions followed by short periods (0.5 min) of rich combustion conditions [3] The temperature is at about 650 °C in order to achieve a partial regeneration. Arosio et al found that the SO<sub>2</sub>-aged Pd/Al<sub>2</sub>O<sub>3</sub> could not be regenerated by  $CH_4$  at temperatures up to 500 °C [7]. Based on this work, the sulfates on PdO<sub>x</sub> particles can be reduced at 400 ℃ by CO and hydrocarbons, which are typical components under rich combustion conditions of NG engines. Unfortunately the advantage of the sulphur-free PdOx is short lived due to migration of sulphur from the alumina support on to the PdOx particle.

# CONCLUSIONS

Sulfur poisoning and regeneration of  $Pd/Al_2O_3$  were performed under simulated lean and rich conditions. The SO<sub>2</sub> adsorption gets saturated quickly (30 min) in the presence of 100 ppm SO<sub>2</sub>, and the oxidation activity deactivates and stabilizes even faster. The support Al<sub>2</sub>O<sub>3</sub> accommodates more than 80% adsorbed sulfur.

Under rich conditions, sulfates on  $PdO_x$  particles  $[PdSO_4]$  are quickly reduced and released from the catalyst as  $SO_2$ . Sulfates on alumina  $[Al_2(SO_4)_3]$  cannot be removed in a reasonable time at temperatures below 550 °C. Under lean conditions, the sulfates on alumina migrate to  $PdO_x$  particles and cause rapid deactivation even without sulfur in the gas stream.

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